KUNKLE SAFETY AND RELIEF PRODUCTS
TECHNICAL REFERENCE


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## Definitions and Commonly Used Terms

## A.S.M.E.

American Society of Mechanical Engineers.

## A.P.I.

American Petroleum Institute

## PRV

Relief Valve, Safety Valve, Safety Relief Valve.

## Back Pressure

The pressure that exists at the outlet of a pressure relief device as a result of the pressure in the discharge system. It is the sum of the superimposed and built-up back pressures.

## Built-up Back Pressure

The increase in pressure in the discharge header that develops as a result of flow after the pressure relief device opens.

## Blowdown

The difference in pressure between the opening pressure and reclose pressure. May be expressed in percent of set pressure or "psig."

## Body/Nozzle/Seat

The stationary seating surface, the inlet.

## Cap

The pressure screw cover and/or lever housing. May be screwed, bolted, packed, or plain lever.

## Chatter

Abnormal, rapid reciprocating movement of the disc on the seat of a pressure relief valve.

## Coefficient of Discharge

The ratio of the measured relieving capacity to the theoretical relieving capacity.

## Disc

The moveable seating surface.

## Gag

A device attached to a safety or safety relief valve that prevents it from opening at the set pressure.

## Guide

That portion of the valve used to guide the disc.

## Lift

The distance between the seat and disc seating surfaces when the valve is in the full open position.

## MAWP

Maximum allowable working pressure. This data is found on the pressure vessel nameplate and is the maximum pressure at which the lowest set safety valve must be set (stamped).

## N.B.

National Board of Boiler and Pressure Vessel Inspectors.

## Operating Pressure

The gauge pressure at which a pressure vessel is maintained in normal operation. The operating pressure should not be in excess of 90 percent of the PRV set pressure.

## Accumulation

The permitted increase in pressure developed after the valve has opened. Usually expressed in percentage, maximum allowable accumulations are established by applicable codes for operating and fire contingencies.

## Pre-open/Warn

An audible or visual discharge at a pressure slightly lower than the set pressure. Warns the operator that the valve is about to operate.

## Pressure Relief Device

A device actuated by inlet static pressure and designed to open during an emergency or abnormal condition to prevent a rise of internal fluid pressure in excess of a specified value. The device may also be designed to prevent excessive internal vacuum. The device may be a pressure relief valve, a non-reclosing pressure relief device, or a vacuum relief valve.

## psia

Pounds per square inch absolute or absolute pressure. Absolute pressure is equal to gauge pressure plus atmospheric pressure (14.7 psi [1.01 barg] at sea level).

## psig

Pounds per square inch gauge or gauge pressure. Differential pressure across the valve, equal to absolute pressure inside the pressure vessel minus atmospheric pressure (14.7 psi [1.01 barg] at sea level).

## Relief Valve

A spring-loaded pressure relief valve actuated by the static pressure upstream of the valve. The valve opens normally in proportion to the pressure increase over the opening pressure. A relief valve is used primarily with incompressible fluids (liquids).

## Safety Relief Valve

A spring-loaded pressure relief valve that may be used as either a safety or relief valve depending on the application.

## Safety Valve

A spring-loaded pressure relief valve actuated by the static pressure upstream of the valve and characterized by rapid opening or pop action. A safety valve is normally used with compressible fluids.

## Set Pressure

The gauge pressure at which a safety valve visibly and audibly opens or at which a relief valve discharges a 1 " long unbroken stream of liquid.

## Spindle/Stem

The rod connecting to the disc.

## Stamped Capacity

The rated relieving capacity that appears on the device nameplate. The stamped capacity is based on the set pressure or burst pressure plus the allowable overpressure for compressible fluids and the differential pressure for incompressible fluids.

## Superimposed Back Pressure

The static pressure that exists at the outlet of a pressure relief device at the time the device is required to operate. It is the result of pressure in the discharge system coming from other sources and may be constant or variable.

## Warn Ring or Regulator Ring

The control ring which surrounds the seat, used to control preopen and blowdown.

## Yoke/Bonnet

The portion of a safety/relief valve that surrounds the spring; the spring housing.

## ASME Codes

The ASME (American Society of Mechanical Engineers) boiler and pressure vessels code requirements for overpressure protection as they relate to Kunkle products is as follows:

## ASME Section I

This code applies to boilers where steam or other vapor is generated at a pressure of 15 psig [1.03 barg] or greater and high temperature water boilers intended for operation at pressures exceeding 160 psig [11.03 barg] and/or temperatures exceeding $250^{\circ} \mathrm{F}\left[121^{\circ} \mathrm{C}\right]$.

## Boiler Pressure Accumulation

No more than 6 percent above the highest pressure at which any valve is set, or no more than 6 percent above MAWP.

## Set Pressure

The set pressure of a one valve installation cannot be higher than the MAWP. The set pressure of the second or other valves in a multiple valve installation can be up to 3 percent above the MAWP. The complete range of valve settings for multiple valve installations cannot be greater than 10 percent of the highest set pressure. For high temperature water boilers, this 10 percent range may be exceeded.

## ASME Section IV

This code applies to steam boilers operating at pressures not greater than $15 \mathrm{psig}[1.03$ barg] and hot water heating boilers operating at pressures not greater than 160 psig [11.03 barg] and/or temperatures not exceeding $250^{\circ} \mathrm{F}\left[121^{\circ} \mathrm{C}\right.$.

## Steam Boilers

Valve capacity must be selected to prevent the boiler pressure from rising more than 5 psig [0.35 barg] above the MAWP.

## Hot Water Boilers

Safety valve must be set to relieve at a pressure not greater than the MAWP of the boiler. If more than one safety valve is used, the secondary valve(s) may be set up to 6 psig [0.41 barg] above the MAWP for boilers with MAWPs up to and including 60 psig [4.13 barg], and 5 percent for boilers with MAWPs greater than 60 psig [ 4.13 barg]. Capacity must be selected to prevent the pressure from rising more than 10 percent above the set pressure of the highest set valve if more than one valve is used.

## Tanks/Heat Exchangers High Temperature Water-to-Water Heat Exchangers

Valve(s) must be set at a pressure not greater than the MAWP and with sufficient capacity to prevent the pressure from increasing more than 10 percent above the MAWP.

## Steam to Hot Water Supply

Valve(s) must be a least 1 " [25 mm] diameter with set pressure not greater than MAWP of the tank.

## High Temperature Water to Steam Heat Exchanger

Valve(s) must be set at a pressure not greater than 15 psig [1.03 barg] and with sufficient capacity to prevent the pressure from rising more than 5 psig [ 0.35 barg] above the MAWP.

## ASME Section VIII

This code applies to unfired pressure vessels with an inside diameter larger than 6" [130 mm ] and designed for use at or above 15 psig [1.03 barg]. Valve(s) must prevent the pressure from rising more than 10 percent or 3 psig [0.21 barg], whichever is greater, above the MAWP. For a single valve installation, the set pressure may not be greater than the MAWP. For multiple valve installations, the first valve cannot be set higher than the MAWP, but the other valves can be set up to 5 percent above the MAWP. The pressure rise for multiple valve installations can be 16 percent or 4 psig [0.27 barg], whichever is greater. When the vessel is exposed to an external heat source, such as fire, the pressure rise can be 21 percent above the MAWP.

## Notes:

1. MAWP - Maximum allowable working pressure.
2. Information stated above is based on latest code at time of publication.

## ASME Codes - Requirements

## National Board

Kunkle valves are manufactured at facilities that meet the manufacturing requirements of the ASME Sections I, IV, and VIII codes for pressure relief valves. Valves that have the relief capacity certified by the National Board of Boiler and Pressure Vessel Inspectors bear the following code symbol stamp on the nameplate and the letters NB. Most Kunkle Valves have NB certified capacities.

## Code Stamps

"V"


HV"


HV
"UV"

applies to all ASME Section I valves
applies to all ASME Section IV valves

Notes:

1. Information stated above is based on latest code at time of publication.
2. Non-code liquid valves are capacity rated at 25 percent overpressure.
3. Non-code air/gas/vapor and steam valves are capacity rated at 10 percent overpressure.

Power Boiler - Section I-Code "V"

| Set Pressure <br> psig |  | [barg] | Set Pressure <br> Tolerance | Minimum <br> Blowdown |
| :--- | :--- | :--- | :--- | :--- |
| $15-100$ | $[1.03-6.90]$ |  |  | Overpressure ${ }^{1}$ |
| $101+$ | $[6.96+]$ |  | 2 psig $[0.14$ barg $]$ min. |  |
| $15-70$ | $[1.03-4.83]$ | $\pm 2$ psig | $[ \pm 0.14$ barg $]$ |  |
| $71-300$ | $[4.90-20.69]$ | $\pm 3 \%$ |  |  |
| $301-1000$ | $[20.95-68.96]$ | $\pm 10$ psig | $[ \pm 0.69$ barg $]$ |  |
| 1001 and up | $[69.03$ and up] $]$ | $\pm 1 \%$ |  |  |

## Notes:

1. Overpressure would be 2 psig [0.14 barg] for pressures between $15-66 \mathrm{psig}[1.03-4.55$ barg]. Pressures above 66 psig [ 4.55 barg] would have an overpressure of $3 \%$.
2. Maximum blowdown is $10 \%$ for "Special Application Section I" valves.

Heating Boiler - Section IV - Code "HV"

|  | Set Pressure <br> psig <br> [barg] |  | Set Pressure <br> Tolerance | Blowdown | Overpressure |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 15 psig <br> Steam | 15 | $[1.03]$ | $\pm 2 \mathrm{psig}$ <br> $[ \pm 0.14 \mathrm{barg}]$ | $2-4 \mathrm{psig}$ <br> $[0.14-0.28 \mathrm{barg}]$ | 5 psig <br> $[0.34 \mathrm{barg}]$ |
| Hot Water | $15-60$ | $[1.03-4.14]$ | $\pm 3 \mathrm{psig}$ <br> $[ \pm 0.21 \mathrm{barg}]$ | $\mathrm{N} / \mathrm{A}$ | $10 \%$ |
| Hot Water | $61-160$ | $[4.20-11.0]$ | $\pm 5 \%$ | $\mathrm{~N} / \mathrm{A}$ | $10 \%$ |

Unfired Pressure Vessel - Section VIII - Code "UV"

| Set Pressure <br> psig | Set Pressure <br> Tolerance | Blowdown | Overpressure |  |
| :--- | :--- | :--- | :--- | :--- |
| $15-30$ | $[1.03-2.07$ barg] | $\pm 2 \mathrm{psig}[ \pm 0.14$ barg] | N/A | $3 \mathrm{psig}[0.21 \mathrm{barg}]$ |
| $31-70$ | $[2.14-4.83$ barg] | $\pm 2 \mathrm{psig}[ \pm 0.14 \mathrm{barg}]$ | $\mathrm{N} / \mathrm{A}$ | $10 \%$ |
| 71 and up [4.90 barg and up] | $\pm 3 \%$ | $\mathrm{~N} / \mathrm{A}$ | $10 \%$ |  |

## Non-code Set Pressure Tolerance

Set Pressure, psig [barg]

## Set Pressure Tolerance, psig [barg]

| Below 15 psig [1.03 barg] to 10 psig [0.69 barg] | +/- 2.0 psig [ $\pm 0.14$ barg] |
| :---: | :---: |
| Below 10 psig [0.69 barg] to 5.0 psig [0.34 barg] | +/- $1.0 \mathrm{psig}[ \pm 0.07 \mathrm{barg}]$ |
| Below 5.0 psig [0.34 barg] to 0.0 psig [0.0 barg] | +/- 0.5 psig [ $\pm 0.003 \mathrm{barg}]$ |
| Below 0.0-inch Hg [0.0 mb] to 10-inch Hg [337 mb] | +/- 1.0-inch Hg [ $\pm 33.7 \mathrm{mb}$ ] |
| Below 10-inch Hg [337 mb] to 20-inch Hg [674 mb] | +/- 2.0-inch Hg [ $\pm 67.4 \mathrm{mb}$ ] |
| Below 20-inch Hg [674 mb] | +/- 4.0-inch Hg [ $\pm 134.8 \mathrm{mb}]$ |

## General Safety and Relief Valve Information

## Kunkle Factory Standard Seat Tightness

| Code Section | Service | Performance Standard |
| :--- | :--- | :--- |
| I and VIII | Steam | No visible leakage for 15 seconds at 20\% below nameplate <br> set pressure or at 5 psig [0.35 barg] below nameplate set <br> pressure, whichever is greater. |
| VIII | Air/Gas | No audible leakage for 15 seconds at 20\% below nameplate <br> set pressure or at 5 psig [0.35 barg] below nameplate set <br> pressure, whichever is greater. |
| IV and VIII | Liquid | No visible leakage for 30 seconds at 20\% below nameplate <br> set pressure or at 5 psig [0.35 barg] below nameplate set <br> pressure, whichever is greater. |
| IV | Steam | No visible leakage for 30 seconds at 12 psig [0.83 barg]. |

## API-527 Seat Tightness

| Model | Code Section | Service | Performance Standard |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & 300 / 600 \\ & 6000 \\ & 900 \end{aligned}$ | I and VIII | Steam | API 527 - No visible leakage for 1 minute at $10 \%$ below nameplate set pressure or 5 psig [ 0.35 barg ] below nameplate set pressure, whichever is greater. |
| 6010 (O-ring seat) 916/917 (soft seat) 918/919 (soft seat) | VIII | Air/Gas | API 527 - Bubble-tight for 1 minute at $10 \%$ below nameplate set pressure or 5 psig [ 0.35 barg] below nameplate set pressure, whichever is greater. |
| $\begin{aligned} & 910 / 912 \\ & 911 / 913 \end{aligned}$ | VIII | Air/Gas | API 527 - D and E orifice: 40 bubbles/min, F thru J orifice: 20 bubbles/min at $10 \%$ below nameplate set pressure or 5 psig [ 0.35 barg] below nameplate set pressure, whichever is greater. |
| $\begin{aligned} & \text { 916/917 (soft seat) } \\ & \text { 918/919 (soft seat) } \end{aligned}$ | VIII | Liquid | API 527 - No leakage for 1 minute at $10 \%$ below nameplate set pressure, or 5 psig [ 0.35 barg] below nameplate set pressure, whichever is greater. |
| $\begin{aligned} & 910 / 912 \\ & 911 / 913 \end{aligned}$ | VIII | Liquid | API 527-10 cc/h for inlet sizes less than 1 " or $10 \mathrm{cc} / \mathrm{h} /$ in of inlet valve size for inlet sizes $1^{\prime \prime}$ and larger at 10\% below nameplate set pressure or 5 psig [0.35 barg] below nameplate set pressure, whichever is greater. |

## Note:

API 527 is not available on air service for:
a. Plain lever "J" orifice Models 900 and 6000.
b. Plain lever Model 900 above 444 psig
[30.6 barg ] set pressure.

The terms "safety valve" and "relief valve" are frequently used interchangeably. This is satisfactory to the extent that both safety and relief valves of the spring-loaded type are similar in external appearance and both serve the broad general purpose of limiting media (liquid or gaseous) pressures by discharging some of the pressurized liquid or gas. Some authorities restrict "safety valves" to those installed on boilers, superheaters, and fired vessels - all others being classified as relief valves. We prefer, however, to define them briefly as follows:

Safety valves are used on gaseous service (which include air and steam). Their design always includes a huddling chamber which utilizes the expansion forces of these gases to effect quick opening (popping) and closing actions. The difference between the opening and closing pressures is termed "blowdown," and for Section I and IV steam safety valves blowdown limitations are carefully stated in the ASME Power Boiler Code. Relief valves are normally used for liquid service, although safety valves may be so used. Ordinarily, relief valves do not have an accentuated huddling chamber nor a regulator ring for varying or adjusting blowdown. They therefore operate with a semi-modulating action in proportion to the system pressure. Such relieving action is desirable to protect piping systems from water hammer.

## Safety and Relief Valve Pointers

1. ASME Codes require that steam and air safety valves have test levers, although levers may be omitted on valves used in hazardous or toxic gas service.
2. Steam safety valves may be used for air service but not vice versa. Liquid valves should be used on liquid only.
3. Safety/relief valves should be installed vertically with the drain holes open or piped to a convenient location.
4. The inlet to and outlet from a safety/relief valve must be at least as large as the valve connections.
5. Every safety/relief valve is individually tested and set by Kunkle.
6. In the event you have safety/relief valve problems, first check the accuracy and cleanliness of pressure gauges and then refer to "Recommended Installation" for help in determining the cause of your problem. Feel free to consult your sales representative.
7. When ordering, we need to know size, type of connections, model number, pressure setting, required relieving capacity, and service media, or advise your complete requirements so that we can make a selection for you.
8. Following are procedures on the operation and testing of safety/relief valves:
A. Avoid excessive operation of the safety/relief valve as even one opening can provide a means for leakage. Safety/relief valves should be operated only often enough to assure that they are in good working order.
B. Test the valve by raising the operating pressure to the set pressure of the safety/relief valve, allowing it to open and reset as it would in normal service.
C. Do not hand operate the valve with less than 75 percent of the stamped set pressure exerted on the underside of the disc. When hand operating, be sure to hold the valve in an open position long enough to purge accumulated foreign material from the seat area and then allow the valve to snap shut.

## Safety and Relief Valve Principles of Operation

Kunkle direct spring operated pressure relief valves consist of a nozzle threaded into a cast body housing which is flanged to a pressurized system. A disc is held against the nozzle by a spring, which is contained in a bonnet. The spring is adjusted by a compression screw to permit the calibration of opening or set pressure. An adjustable nozzle ring, threaded onto the nozzle,

controls the geometry of the fluid exit control chamber (huddling chamber). The huddling chamber geometry is very important in controlling valve opening and closing pressures, and stability of operation. The nozzle ring is locked into position by a ring pin assembly. A cap attached to the top of the bonnet seals the internal calibration adjustments. Refer to the illustration above for the location of these important components.
Under normal system operation the valve remains in the closed position because the spring force (Fs) is greater than the system pressure acting on the internal nozzle seating area (PA). If system pressure increases to a point when these forces are equal, the valve begins to simmer. The disc lifts and fluid flows through the valve. When
pressure in the system returns to a safe level, the valve closes.

Just prior to reaching set point, the pressure relief valve leaks system fluid into the huddling chamber. The fluid now acts on a larger area of the disc inside the huddling chamber (PAh), causing the valve to experience an instantaneous increase in the opening force. Refer to the Figure on page 7 to see relationship between Nozzle Area (A) and the Huddling Chamber Area (Ah). System pressure acting on the larger area will suddenly open the pressure relief valve at a rapid rate.
Although the opening is rapid and dramatic, the valve does not open fully at set point. The system pressure must increase above the set point to open the valve to its full lift and full capacity position. Maximum lift and certified flow rates will be achieved within the allowable limits (overpressure) established by various codes and standards. All pressure relief valves are allowed an overpressure allowance to reach full rated flow.


Pressure Force PA

## Safety and Relief Valve Principles of Operation



Relationship of Nozzle Area to Huddling Chamber Area

Once the valve has controlled the pressure excursion, system pressure will start to reduce. Since the huddling chamber area is now controlling the exit fluid flow, system pressure must reduce below the set point before the spring force is able to close the valve. The difference between the set pressure and the closing pressure is called blowdown, and is usually expressed as a percentage of set pressure. Refer to code for appropriate blowdown.


Valve Opens, Force $\mathrm{P}_{\text {Ah }}$ Acting on Disc

The nozzle ring adjustment changes the shape and volume of the huddling chamber, and its position will affect both the opening and closing characteristics of the valve. When the nozzle ring is adjusted to its top position, the huddling chamber is restricted to its maximum. This ring position will usually make the valve pop very distinctly with a minimum simmer (leakage before opening), but the blowdown will increase. When the nozzle ring is lowered to its lowest position, minimal restriction to the huddling chamber occurs. At this position, simmer increases and the blowdown decreases. The final ring position is somewhere between these two extremes to provide acceptable performance.

## Liquid Service Operation

On liquid service, a different dynamic situation exists. Liquids do not expand when flowing across orifices, and a small amount of fluid flow across the nozzle will produce a large local pressure drop at the nozzle orifice. This local pressure drop causes the spring to reclose the valve if the fluid flow is minimal. Liquids leaking into the huddling chamber can quickly drain out by gravity and prevent fluid pressure from building up on the secondary area of the huddling chamber. Liquid relief valves are thus susceptible to a phenomenon called chatter, especially at low fluid flow rates. Chatter is the rapid opening and closing of the pressure relief valve and is often destructive in nature.
Since no visible or audible pop is heard at set point, liquid set pressure is defined as the pressure when the first heavy flow occurs (first steady vertical flow).

## Ordering Information

Purchase orders must show the Size, Model Number, Set Pressure, and Service. (Include flange rating with size when applicable.)

1. To make a proper catalog selection, the following information will be needed:
A. Connection sizes (in and out), and types (male, female, flanged; 125\#, 150\#, 250\#, 300\#, etc.)
B. Material of construction
a. Bronze
b. Iron
c. Steel
d. Stainless Steel or other
C. Pressure setting
D. Service (steam, air, gas, etc., including any applicable codes or standards)
E. Capacity required, if available
F. Unusual conditions (temperature, location, etc.)

Be sure to use the capacity correction factors for superheated steam, liquid overpressure (10 percent), air-gas temperature and density correction.
G. If valve is to be "equal to" another brand, provide nameplate information or specification data from brand being replaced.
2. Ordering data for replacement valves may be obtained from the valve nameplate or stamping.

## Valve Selection

The most critical consideration when selecting a pressure relief valve is that the valve will be capable of passing the maximum expected flow capacity. To properly select a relief valve the user must first determine the following:

1. The set pressure at which the valve is to operate. This pressure is based on the pressure limits of the system and the applicable codes. The set pressure of the primary pressure relief valve must not exceed the maximum allowable pressure of the system, but should be at least 10 percent above the maximum operating pressure.
2. The physical properties of the fluid media to be relieved. Capacity values are given in the Kunkle catalogs based on air, saturated steam, and water. Kunkle valves will relieve many other fluids, but information such as molecular weight, specific gravity, viscosity, ratio of specific heats, compressibility factor, and process temperature may be necessary to insure accurate valve selection.
3. The required relieving capacity. The ASME Boiler and Pressure Vessel Code, American Petroleum Institute Recommended Practices, and other applicable standards have many rules for obtaining the required relieving capacity and should be referenced when making this determination. The user must consider all sources of pressure generation in the system that will be protected by the pressure relief valve. Examples of pressure generation sources are pumps, heat input that may cause the system fluid to boil or expand, etc. The pressure relief valve(s) selected must exceed the worst case source of flow generation to prevent the system pressure from exceeding acceptable limits.

Once the previous information has been collected, the pressure relief valve may be sized by using the capacity charts lincluded in each model's catalog sheet) or by performing sizing calculations (see Valve Sizing, pages 14-25). The user will also want to consider other important factors such as:

- Connection size and type. This information is given in the Valve Selection Guide and in each of the Model Catalog sheets. Please note that the inlet to and outlet from a pressure relief valve must be at least as large as the valve connections to prevent valve malfunction.
- Pipe Size. Connection pipe sizes should not be determined by equipment connections, but rather by the relieving capacity of the PRV.
- Applicable code compliance. The ASME Code Summary section gives important information about pressure relief valves from the code. Pressure relief valve users are strongly encouraged to reference the full version of the code for important rules that may not be included in this manual.
- Maximum allowable seat leakage. The General Safety and Relief Valve Information (page 6) section of this manual shows the leakage acceptance criteria applied to each Kunkle valve. Pressure relief valve users should keep in mind that if "zero leakage" is a requirement, a soft seated valve must be selected.
- Environmental conditions. Environmental conditions play a significant role in how pressure relief valves operate. Extremely high ambient temperatures may affect the set pressure of the valve, extremely low temperatures combined with moisture can cause valves to "freeze up" and prevent proper operation, and vibration may severely shorten the service life of the valve. The Valve Selection Guide (pages 11-13) in this manual has general information on the pressure and temperature limits for each valve series. For specific model limitations refer to the individual model catalog. For vibration service, please contact your local Kunkle representative for assistance.
- Valve options. Each Kunkle model is offered with useful options such as pressure tight caps, lift lever options, or vibration dampening preparation. When selecting valve options, keep in mind that there are code requirements that may dictate what options may be used. For instance the ASME code dictates that all air, steam and hot water $\left(140^{\circ} \mathrm{F}+\left[60^{\circ} \mathrm{C}+\right]\right)$ pressure relief valves must be equipped with a lift lever. Refer to the individual model catalogs for listings of available options.
- Installation space. The individual model catalogs show envelope dimensions for each configuration and size.
For assistance on valve sizing and selection, please contact your local sales representative.

Valve Selection Guide
(For specific minimum/maximum temperature/pressure ranges refer to individual product sections.)
Steam (ASME Section I - Power Boilers)

| Model(s) | Material Connections |  |  |  | Inlet Size Range in [mm] |  | Min/Max ${ }^{1}$ Press. psig [barg] |  | Min/Max Temp. ${ }^{\circ} \mathrm{F} \quad\left[{ }^{\circ} \mathrm{C}\right]$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Body | Trim | NPT | FLGD |  |  |  |  |  |  |
| 300, 600 | CS | SS |  | X | 11/4-6" | [31.75-152.4] | 15/1000 | [1.0/69] | -20/800 | [-29/427] |
| $920,921,927$ <br> (special use - 10\% blowdown) | ${ }_{\text {) }} \mathrm{CS}$ | SS | X |  | 1/2-2" | [12.7-50.8] | 15/1400 | [1.0/96.5] | -20/800 | [-29/427] |
| $\begin{aligned} & \text { 6010, 6021, 6121, } 6182 \\ & 6186,6221,6283 \end{aligned}$ | Bronze | Brass | X |  | 1/2-21/2" | [12.7-63.5] | 3/250 | [0.69/17.2] | -60/406 | [-51/208] |
| 6030, 6130, 6230 | Bronze | SS | $x$ |  | $1 / 2-21 / 2^{\prime \prime}$ | [12.7-63.5] | 3/300 | [0.69/20.7] | -60/425 | [-51/219] |
| 6252 | Iron | SS | X | X | 11/2-6" | [38.1-152.4] | 10/250 | [0.69/17.2] | -20/406 | [-29/208] |

Steam (ASME Section VIII - Unfired Steam Equipment)

| 1 and 2 | Bronze | Brass | $X$ |  | 1/2-1" | [12.7-25.4] | 5/250 | [0.34/17.2] | -60/406 | [-51/208] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 264, 265 | CS | SS | $X$ |  | 1/2-1" | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 266, 267 | SS | SS | $X$ |  | 1/2-1" | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 300,600 | CS | SS |  | X | $11 / 4-6 "$ | [31.75-152.4] | 15/1000 | [1.0/69] | -20/750 | [-29/399] |
| 910 | CS | SS | $x$ | 0 | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -20/800 | [-29/427] |
| 911 | SS | SS | $X$ | 0 | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -320/800 | -195/427] |
| 912 | Bronze | Brass | $x$ |  | 1/2-2" | [12.7-50.8] | 3/250 | [0.21/17.2] | -320/406 | [-195/208] |
| 913 | Bronze | SS | $X$ |  | 1/2-2" | [12.7-50.8] | 3/300 | [0.21/20.7] | -320/425 | -195/219] |
| $\begin{aligned} & \text { 6010, 6021, 6121, 6182, } \\ & 6186,6221,6283 \end{aligned}$ | Bronze | Brass | X |  | 1/2-21/2" | [12.7-63.5] | 3/250 | [0.21/17.2] | -60/406 | [-51/208] |
| 6030, 6130, 6230 | Bronze | SS | X |  | $1 / 2-21 / 2^{\prime \prime}$ | [12.7-63.5] | 3/300 | [0.21/20.7] | -60/425 | [-51/219] |
| 6252 | Iron | SS | X | X | 11/2-6" | [38.1-152.4] | 10/250 | [0.69/17.2] | -20/406 | [-29/208] |

Steam (ASME Section IV - Low Pressure Steam Heating Boilers)

| 930 | Iron | Bronze | $x$ |  | 2-3" | [50.8-76.2] | 15 only | [1.0] | 250 only | [122] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6933, 6934 | Bronze | Brass | $x$ |  | 1/2-2" | [12.7-50.8] | 15 only | [1.0] | 250 only | [122] |
| 6935 | Bronze | SS | $x$ |  | 1/2-2" | [12.7-50.8] | 15 only | [1.0] | 250 only | [122] |
| 6254 | Iron | SS | $X$ | $X$ | 11/2-6" | [38.1-152.4] | 15 only | [1.0] | 250 only | [122] |

## Steam (Non-code)2

40R, 40RL SS SS X $\quad \mathrm{S} \quad 1 / 2-3 / 4^{\prime \prime} \quad[12.7-19.05] \quad 1 / 400 \quad[0.07 / 27.6] \quad-60 / 850 \quad[-51 / 454]$
$X=$ Standard $\quad O=$ Optional

## Notes:

[^0]
## Valve Selection Guide

(For specific minimum/maximum temperature/pressure ranges refer to individual product sections.)

## Air/Gas (ASME Section VIII)

| Model(s) | Material |  | Connections |  | Inlet Size Range in [mm] |  | Min/Max ${ }^{3}$ Press. psig [barg] |  | Min/Max4 Temp. ${ }^{\circ} \mathrm{F}$ <br> [ ${ }^{\circ} \mathrm{C}$ ] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 and 2 | Brass | Brass | $X$ |  | $1 / 2-1^{\prime \prime}$ | [12.7-25.4] | 5/250 | [0.34/17.2] | -60/406 | [-51/208] |
| 30 | Brass | Brass | $X$ |  | $1 / 4^{\prime \prime}$ | [6.35] | 60/4000 | [4.1/275.8] | 20/300 | [-6.6/150] |
| 189 | Bronze | SS | $X$ |  | 1/2-3/4" | [12.7-19.05] | 1000/2500 | [69/344.8] | -320/350 | [-195/177] |
| 264, 265 | CS | SS | $X$ |  | $1 / 2-1^{\prime \prime}$ | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 266, 267 | SS | SS | X |  | $1 / 2-1^{\prime \prime}$ | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 300, 600 | CS | SS |  | X | 11/4-6" | [31.75-152.4] | 15/1000 | [1.0/69] | -20/800 | [-195/427] |
| 3305 | Aluminum | mS | X |  | 1/4" | [6.35] | 1000/5500 | [69/379.3] | -20/185 | [-29/85] |
| 330S, 333S ${ }^{5}$ | Aluminum | m SS |  |  | $1 / 4^{\prime \prime}$ | [6.35] | 2000/6500 | [138/448.3] | -20/185 | [-29/85] |
| 337 | Iron | Bronze | X |  | 2-3" | [50.8-76.2] | 1/60 | [0.07/4.14] | -20/406 | [-29/208] |
| 338 | Aluminum | Brass | $X$ |  | 2 " | [50.8] | 5/30 | [0.3/2.07] | -30/400 | [-34/204] |
| 363 | Bronze | SS | $X$ |  | $1 / 2-3 / 4{ }^{\prime \prime}$ | [12.7-19.05] | 50/1000 | [3.4/69] | -320/350 | [-195/177] |
| 389 | SS | SS | $X$ |  | 1/2-3/4" | [12.7-19.05] | 50/2500 | [3.4/172.4] | -320/350 | [-195/177] |
| 541 (Buna disc), 542 (Viton® disc), 548 (SS disc) | Brass | Brass | X |  | 1/4-1/2" | [6.35-12.7] | 3/400 | [0.21/27.6] | -20/400 | [-29/204] |
| 910, 916 (soft seat) ${ }^{4}$ | CS | SS | $X$ | 0 | 1/2-21 | [12.7-50.8] | 3/1400 | [0.21/96.5] | -20/800 | [-29/427] |
| 911, 917 (soft seat) ${ }^{4}$ | SS | SS | $X$ | O | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -320/800 | [-195/427] |
| 912, 918 (soft seat) ${ }^{4}$ | Bronze | Brass | $X$ |  | 1/2-2" | [12.7-50.8] | 3/300 | [0.21/20.7] | -320/406 | [-195/208] |
| 913, 919 (soft seat) ${ }^{4}$ | Bronze | SS | $X$ |  | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -320/425 | [-195/219] |
| $\begin{aligned} & 6010,6121,6182 \\ & 6186,6221,6283^{1} \end{aligned}$ | Bronze | Brass | $X$ |  | $1 / 2-2^{1 / 2 "}$ | [12.7-63.5] | 3/250 | [0.21/17.2] | -60/406 | [-51/208] |
| 6030, 6130, 6320 | Bronze | SS | $X$ |  | 1/2-21/2" | [12.7-63.5] | 3/300 | [0.21/20.7] | -60/425 | [-51/219] |
| 6252 | Iron | SS | $X$ | $X$ | 11/2-6" | [38.1-152.4] | 10/250 | [0.69/17.2] | -20/406 | [-29/208] |

## Air/Gas2 (Non-code)

| 230 (Kynar® ${ }^{\circledR}$ seat) | Aluminum SS | X | $1 / 4^{\prime \prime}$ | $[6.35]$ | $300 / 1500$ | $[20.7 / 103.4]$ | $-20 / 185$ | $[-29 / 85]$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 803 (Kynar® seat) | Aluminum SS | X | $1 / 4^{\prime \prime}$ | $[6.35]$ | $1000 / 6000$ | $[69 / 413.8]$ | $-20 / 185$ | $[-29 / 85]$ |  |
| 818 (Teflon ${ }^{\circledR}$ seat) | CS | SS/Brass X | $2^{\prime \prime}$ | $[50.8]$ | $120 / 150$ | $[8.3 / 10.3]$ | $-20 / 300$ | $[-29 / 150]$ |  |


| Air/Gas (Vacuum) in Hg [mm Hg] |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 215 V | Iron | Bronze | X |  | 2-3" | [50.8-76.2] | 2/29 | [50/736] | -20/406 | [-29/208] |
| 910, 916 (soft seat) ${ }^{4}$ | CS | SS | $x$ | 0 | 1/2-2" | [12.7-50.8] | 6/29 | [152/736] | -20/800 | [-29/427] |
| 911, 917 (soft seat) ${ }^{4}$ | SS | SS | X | 0 | 1/2-2" | [12.7-50.8] | 6/29 | [152/736] | -320/800 | [-195/427] |
| 912, 918 (soft seat) ${ }^{4}$ | Bronze | Brass | X |  | 1/2-2" | [12.7-50.8] | 6/29 | [152/736] | -320/406 | [-195/208] |
| 913, 919 (soft seat) ${ }^{4}$ | Bronze | SS | X |  | 1/2-2" | [12.7-50.8] | 6/29 | [152/736] | -320/425 | [-195/219] |

$X=$ Standard $\quad O=$ Optional

## Notes:

1. Soft seat available on some models.
2. See also Section VIII air valves for non-code air/gas applications.
3. Set pressures less than 15 psig [1.0 barg] are non-code only.
4. Temperature limits of soft seats determine operating limits of valve.
5. Kynar ${ }^{\circledR}$ or Urethane Seat.

## KUNKLE SAFETY AND RELIEF PRODUCTS

TECHNICAL REFERENCE

## Valve Selection Guide

(For specific minimum/maximum temperature/pressure ranges refer to individual product sections.)

| Liquid (ASME Section IV - Hot Water Boilers) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model(s) | $\begin{array}{r} \text { Ma } \\ \text { Body } \end{array}$ | rial Trim | Connections <br> NPT FLGD | Inlet in | Size Range [mm] | $\begin{gathered} \text { Min/Max } \\ \text { psig } \end{gathered}$ | Press. <br> [barg] | $\underset{{ }^{\circ} \mathrm{F}}{\mathrm{Min}} / \mathrm{M}$ | $x^{2}$ Temp. [ ${ }^{\circ} \mathrm{C}$ ] |
| 537 (soft seat) | Iron/B | onze | Brass $X$ | $3 / 4-2{ }^{\prime \prime}$ | [19.05-50.8] | 15/160 | [1.0/11] | -20/250 | [-29/121] |


| Liquid (ASME Section VIII) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 910, 916 (soft seat) ${ }^{2}$ | CS | SS | x | 0 | 1/2-2" | [12.7-50.8] | 3/1400 [0.21/96.5] | -20/800 | [-29/427] |
| 911, 917 (soft seat) ${ }^{2}$ | SS | SS | $x$ | 0 | 1/2-2" | [12.7-50.8] | 3/1400 [0.21/96.5] | -320/800 | [-195/427] |
| 912, 918 (soft seat) ${ }^{2}$ | Bronze | Brass | x |  | 1/2-2" | [12.7-50.8] | 3/300 [0.21/20.7] | -320/406 | [-195/208] |
| 913, 919 (soft seat) ${ }^{2}$ | Bronze | SS | x |  | $1 / 2-2{ }^{\prime \prime}$ | [12.7-50.8] | 3/1400 [0.21/96.5] | -320/425 | [-195/219] |


| Liquid (Non-code) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19, 20 | Bronze | Bronze | X | 0 | 1/2-3" | [12.7-76.2] | 1/300 | [0.07/20.7] | -60/406 | [-51/208] |
| 19M, 20M | Bronze | SS | X | 0 | $2^{1 / 2}-3^{\prime \prime}$ | [63.5-76.2] | 1/500 | [0.07/34.5] | -60/406 | [-51/208] |
| 715 | Iron | SS | X |  | 1/2-2" | [12.7-50.8] | 1/250 | [0.07/17.2] | -20/406 | [-29/208] |
| 171, 171P | CS | SS | X |  | 1/2-2" | [12.7-50.8] | 1/400 | [0.07/27.6] | -20/550 | [-29/288] |
| 1715 | SS | SS | X |  | 1/2-2" | [12.7-50.8] | 1/400 | [0.07/27.6] | -20/550 | [-29/288] |
| 91 | Iron | Bronze | X | X | $11 / 2-6 "$ | [38.1-152.4] | 5/400 | [0.34/27.6] | -20/406 | [-29/208] |
| 218,228 | Iron | Bronze | X |  | 3,4 , and $6 "$ | [76.2-152.4] | 60/200 | [4.1/13.8] | -20/406 | [-29/208] |
| 140 | SS | SS | $x$ |  | $3 / 8-1 / 2$ " | [9.5-12.7] | 10/300 | [0.69/20.7] | -60/406 | [-51/208] |
| 264, 265 | CS | SS | X |  | $1 / 2-1{ }^{1 /}$ | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 266, 267 | SS | SS | X |  | $1 / 2-1^{\prime \prime}$ | [12.7-25.4] | 4/3300 | [0.28/227.6] | -20/750 | [-29/399] |
| 910, 916 (soft seat) ${ }^{2}$ | CS | SS | X | 0 | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -20/800 | [-29/427] |
| 911, 917 (soft seat) ${ }^{2}$ | SS | SS | X | 0 | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -320/800 | [-195/427] |
| 912, 918 (soft seat) ${ }^{2}$ | Bronze | Brass | x |  | 1/2-2" | [12.7-50.8] | 3/300 | [0.21/20.7] | -320/406 | [-195/208] |
| 913, 919 (soft seat) ${ }^{2}$ | Bronze | SS | X |  | 1/2-2" | [12.7-50.8] | 3/1400 | [0.21/96.5] | -320/425 | [-195/219] |

Liquid - Underwriters Laboratories (UL) For Oil Services

| 200 A | Bronze | Brass | X |  | $3 / 4-11 / 2^{\prime \prime}$ | $[19.05-38.1]$ | $1 / 200$ | $[0.07 / 13.8]$ | $-60 / 406$ | $[-51 / 208]$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 200 H | Bronze | SS | X | O | $3 / 4-2 "$ | $[19.05-50.8]$ | $1 / 200$ | $[0.07 / 13.8]$ | $-60 / 406$ | $[-51 / 208]$ |

Liquid - Underwriters Laboratories (UL) and Factory Mutual Research (FM) For Fire Pump Water Relief

| 218,228 | Iron | Bronze | $X$ | $X 3,4$ and $6^{\prime \prime}$ | $[76.2-152.4]$ | $60 / 200$ | $[4.1 / 13.8]$ | $-20 / 406$ | $[-29 / 208]$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 918 (soft seat) ${ }^{2,3}$ | Bronze | Brass $\quad$ X | $3 / 4-1^{\prime \prime}[19.05-25.4]$ | $60 / 250$ | $[4.1 / 17.2]$ | $-20 / 406$ | $[-29 / 208]$ |  |  |

Other - Drip Pan Elbow

| 299 | Iron | N/A | X | X | $2-8$ - [50.80-203.2] | N/A | N/A | -20/406 | [-29/208] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## $\mathrm{X}=$ Standard $\quad 0=$ Optional

## Notes:

1. Set pressures below 15 psig [1.0 barg] are
2. Temperature limits of soft seats determine
3. FM Approved only non-code only. operating limits of valve.

## Valve Sizing

After the required relieving capacity has been determined, the pressure relief valve may be sized by using the capacity charts that are included in each model's catalog sheet. The capacities given in those charts may be adjusted for special conditions such as fluid density and temperature by using the correction factors given in Tables B through D (pages 18-20). Valves may also be sized by performing sizing calculations per the formulas (pages 15 and 16) in this section.
Most Kunkle valves may be sized by using the "Coefficient Method" (listed below). These valves typically are high lift valves where the nozzle bore is the flow controlling orifice. This calculation method involves selecting the valve model and corresponding flow coefficient and orifice area from Table A (page 16) and then using the capacity formula (page 14) for the service in which the valve will function.

## IV-A Coefficient Method

Follow these steps for calculating what orifice size is necessary to flow the required capacity:

1. Select the Model Family that you are interested in from the Valve Selection Guide (pages 10-13).
2. From Table A (page 17), record the Flow Coefficient ( $\mathrm{K}_{\mathrm{d}}$ ) corresponding to the service in which the valve will operate.
3. Select the proper formulals) for the service in which the valve will operate. Calculate the minimum required orifice area.
4. Select the Orifice/Size Designation from Table A (page 17) that has a Flow Area closest to, but not less than the minimum required orifice area calculated in step 3 .

Kunkle Models 30, 541, 542, and 548 use the "Slope Method" for sizing calculations. These valves are typically low lift valves, where the annular orifice between the disc and the nozzle seat is the flow controlling orifice. These models are characterized by having a linear increase in capacity with respect to inlet pressure. The "slope" defines this direct relationship of inlet pressure to capacity. Consult your sales representative for sizing assistance.
Kunkle Models 1, 2, 19, 20, 200, 71S, 171, 171S, 91, 218, 228, and 140 use the "KA Method" for sizing calculations. This method is similar to the slope method, in that it is used for low lift valves and is empirically derived. The major difference is that the relationship between inlet pressure and capacity is not linear. These valves are characterized by having low lift that varies with inlet pressure, which makes the flow controlling orifice area indeterminate. Consult your sales representative for sizing assistance.

## KUNKLE SAFETY AND RELIEF PRODUCTS

## TECHNICAL REFERENCE

## Valve Sizing

## U.S. Units

## Metric Units

## Steam - Sections I, IV and VIII (15 psig and above)

$$
A=\frac{W}{51.5 \mathrm{~K}_{\mathrm{d}} \mathrm{P}_{1} \mathrm{~K}_{\text {sh }}} \quad A=\frac{W}{52.5 \mathrm{~K}_{\mathrm{d}} \mathrm{P}_{1} \mathrm{~K}_{\text {sh }}}
$$

## Steam - Non Code (less than 15 psig)

$$
A=\frac{W}{735 F_{2} K_{d}} \quad \sqrt{\frac{T Z}{M P_{1}\left(P_{1}-P_{2}\right)}} \quad A=\frac{W}{558 F_{2} K_{d}} \quad \sqrt{\frac{T Z}{M P_{1}\left(P_{1}-P_{2}\right)}}
$$

## Air - Section VIII (15 psig and above)

$$
A=\frac{V \sqrt{M T Z}}{6.32 \mathrm{C} \mathrm{~K}_{d} \mathrm{P}_{1}} \quad A=\frac{V \sqrt{\mathrm{MTZ}}}{\substack{\text { Volumetric Flow }}} \quad \begin{gathered}
\text { Volumetric Flow }
\end{gathered}
$$

$$
A=\frac{W}{C K_{d} P_{1}} \sqrt{\text { Mass Flow }} \sqrt{\frac{T Z}{M}} \quad A=\frac{1.316 W}{C_{d} P_{1}} \sqrt{\frac{T Z}{M}}
$$

## Air - Non-Code (less than 15 psig)

$A=\frac{V}{4645.2 F_{2} K_{d}} \sqrt{\frac{M T Z}{P_{1}\left(P_{1}-P_{2}\right)}}$
$A=\frac{V}{12503 F_{2} K_{d}} \sqrt{\frac{M T Z}{P_{1}\left(P_{1}-P_{2}\right)}}$

## Liquid - Section VIII (15 psig and above)

$$
A=\frac{Q}{38 K_{d}} \sqrt{\frac{G}{\left(1.1 p_{1}-p_{2}\right)}}
$$

$$
A=\frac{Q}{5.094 K_{d}} \sqrt{\frac{G}{\left(1.1 p_{1}-p_{2}\right)}}
$$

## Liquid - Non-Code

$$
A=\frac{Q}{38 K_{d}} \sqrt{\frac{G}{\left(1.25 p_{1}-p_{2}\right)}}
$$

$$
A=\frac{Q}{5.094 K_{d}} \sqrt{\frac{G}{\left(1.25 p_{1}-p_{2}\right)}}
$$

## $F_{2}$ - Coefficient of Subcritical Flow

$F_{2}=\sqrt{\left(\frac{k}{k-1}\right)(r)^{2 / k}\left[\frac{1-r^{(k-1) / k}}{1-r}\right]}$

## Note:

1. Consult your sales representative for sizing assistance for product groups: Fig. 1 and 2; Fig. 19, 20, 200; Fig. 30; Fig. 71S, 171, 171S; Fig. 91, 218, 228; Fig. 140; and Fig. 541, 542 and 548.

## Valve Sizing

## Sizing Coefficient Method

A = Required effective discharge area of the valve, in ${ }^{2}$ [ $\mathrm{cm}^{2}$ ]
$\mathrm{W}=$ Mass Flow Rate, $\mathrm{lb} / \mathrm{hr}[\mathrm{kg} / \mathrm{hr}]$
$\mathrm{V}=$ Volumetric Flow Rate (gases, vapors) in SCFM [ $\mathrm{Nm} 3 / \mathrm{hr}]$ at standard atmospheric conditions of 14.7 psia and $60^{\circ} \mathrm{F}$ [ 1.013 bara $/ 0^{\circ} \mathrm{C}$ ]

Q = Volumetric Flow Rate (liquids) in GPM [m3/hr] at standard atmospheric conditions of 14.7 psia and $70^{\circ} \mathrm{F}$ [ 1.013 bara $/ 21^{\circ} \mathrm{C}$ ]
$\mathrm{K}_{\mathrm{d}}=$ ASME Flow Coefficient of Discharge
$P_{1}=$ See chart below
$P_{2}=$ Atmospheric Pressure $=14.7$ psia
$p_{1}=$ Set Pressure (psig)
$\mathrm{p}_{2}=$ Back Pressure (psig)
$F_{2}=$ Coefficient of Subcritical Flow
$\mathrm{k}=$ Ratio of Specific Heat-1.31 for Steam, 1.4 for Air
$r=$ Ratio of Back Pressure to Upstream Relieving Pressure $=P_{2} / P_{1}$
M = Molecular Weight of Process Medium
$\mathrm{T}=$ Relieving Temperature, ${ }^{\circ} \mathrm{R}={ }^{\circ} \mathrm{F}+460\left[{ }^{\circ} \mathrm{K}={ }^{\circ} \mathrm{C}+273\right]$
$Z=$ Compressibility Factor (assume $Z=1$ if unknown)
$C=$ Gas Constant based on $k$ (if unknown, use $C=315$ )
$\mathrm{G}=$ Specific Gravity of process fluid at $70^{\circ} \mathrm{F}\left[21^{\circ} \mathrm{C}\right]$
$\mathrm{K}_{\mathrm{sh}}=$ Superheat Steam Correction Factor

## Allowable Overpressure

| Designation | Section | Definition |
| :---: | :---: | :---: |
| $\mathrm{P}_{1}$ | Section I Steam (15 psig and above) | Set pressure $+3 \%$ or 2 psi overpressure (whichever is greater) +14.7 psia |
| $\mathrm{P}_{1}$ | Section IV Steam ( 15 psig and above) | Set pressure +5 psi overpressure +14.7 psia for Low Pressure Steam Boilers |
| $\mathrm{P}_{1}$ | Section IV Hot Water (15 psig and above) | Set pressure + $10 \%$ overpressure +14.7 psia for Hot Water Boilers |
| $\mathrm{P}_{1}$ | Non-Code Steam (below 15 psig) | Set pressure + 10\% overpressure + 14.7 psia |
| $\mathrm{P}_{1}$ | Section VIII Steam (15 psig and above) | Set pressure $+10 \%$ or 3 psi overpressure (whichever is greater) +14.7 psia |
| $\mathrm{P}_{1}$ | Non-Code Air (below 15 psig) | Set pressure + 10\% overpressure + 14.7 psia |
| $\mathrm{P}_{1}$ | Section VIII Air (15 psig and above) | Set pressure $+10 \%$ or 3 psi overpressure (whichever is greater) +14.7 psia |
| $\mathrm{P}_{1}$ | Non-Code Liquid (below 15 psig) | Set pressure (psig) |
| $\mathrm{P}_{1}$ | Section VIII Liquid (15 psig and above) | Set pressure (psig) |

## Valve Sizing

| Table A |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model Family | Orifice/Size <br> Designation | Flow Area in ${ }^{2}$ [ $\left.\mathrm{cm}^{2}\right]$ |  | Non-Code and ASME Section VIII Air/Gas and Steam | Flow Coefficient ( $\mathrm{K}_{\mathrm{d}}$ )  <br> ASME ASME <br> Section I Section IV <br> Steam Steam |  | Non-Code and ASME Section VIII Liquid |
| 189 | $\begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}$ | $\begin{aligned} & 0.034 \\ & 0.034 \end{aligned}$ | $\begin{aligned} & {[0.219]} \\ & {[0.219]} \end{aligned}$ | $\begin{aligned} & 0.874 \\ & 0.874 \end{aligned}$ |  |  |  |
| 264 | $\begin{aligned} & \text { C } \\ & \text { D } \\ & \text { E } \end{aligned}$ | $\begin{aligned} & 0.110 \\ & 0.110 \\ & 0.110 \end{aligned}$ | $\begin{aligned} & {[0.710]} \\ & {[0.710]} \\ & {[0.710]} \end{aligned}$ | $\begin{aligned} & 0.766 \\ & 0.766 \\ & 0.766 \end{aligned}$ |  |  | $\begin{aligned} & 0.408 \\ & 0.408 \\ & 0.408 \end{aligned}$ |
| 337 | $\begin{aligned} & \mathrm{H} \\ & \mathrm{~J} \\ & \mathrm{~K} \end{aligned}$ | $\begin{aligned} & 1.838 \\ & 2.786 \\ & 4.037 \end{aligned}$ | $\begin{aligned} & {[11.858]} \\ & {[17.974]} \\ & {[26.045]} \end{aligned}$ | $\begin{aligned} & 0.860 \\ & 0.860 \\ & 0.860 \end{aligned}$ |  |  |  |
| 537 | $\begin{aligned} & \mathrm{D} \\ & \mathrm{E} \\ & \mathrm{G} \\ & \mathrm{H} \end{aligned}$ | $\begin{aligned} & 0.533 \\ & 0.833 \\ & 1.767 \\ & 3.142 \end{aligned}$ | $\begin{aligned} & {[3.439]} \\ & {[5.374]} \\ & {[11.400]} \\ & {[20.271]} \end{aligned}$ |  |  | $\begin{aligned} & 0.806 \\ & 0.806 \\ & 0.806 \\ & 0.806 \end{aligned}$ |  |
| 910 | $\begin{aligned} & D \\ & \mathrm{D} \\ & \mathrm{~F} \\ & \mathrm{G} \\ & \mathrm{H} \\ & \mathrm{~J} \end{aligned}$ | $\begin{aligned} & 0.121 \\ & 0.216 \\ & 0.337 \\ & 0.553 \\ & 0.864 \\ & 1.415 \end{aligned}$ | $\begin{aligned} & {[0.781]} \\ & {[1.394]} \\ & {[2.174]} \\ & {[3.568]} \\ & {[5.574]} \\ & {[9.129]} \end{aligned}$ | $\begin{aligned} & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \end{aligned}$ | $\begin{aligned} & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \end{aligned}$ |  | $\begin{aligned} & 0.710 \\ & 0.710 \\ & 0.710 \\ & 0.710 \\ & 0.710 \\ & 0.710 \end{aligned}$ |
| 930 | $\begin{aligned} & H \\ & J \\ & \text { K } \end{aligned}$ | $\begin{aligned} & 5.080 \\ & 6.350 \\ & 7.620 \end{aligned}$ | $\begin{aligned} & {[32.774]} \\ & {[40.968]} \\ & {[49.161]} \end{aligned}$ |  |  | $\begin{aligned} & 0.818 \\ & 0.818 \\ & 0.818 \end{aligned}$ |  |
| 6010 | D E F G $H$ $J$ | $\begin{aligned} & 0.121 \\ & 0.216 \\ & 0.337 \\ & 0.553 \\ & 0.864 \\ & 1.415 \end{aligned}$ | $[0.781]$ $[1.394]$ $[2.174]$ $[3.568]$ $[5.574]$ $[9.129]$ | $\begin{aligned} & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \end{aligned}$ | $\begin{aligned} & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \end{aligned}$ | $\begin{aligned} & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \\ & 0.878 \end{aligned}$ |  |
|  | J | 1.414 | [9.123] | 0.878 | 0.878 | 0.878 |  |
|  | K | 2.022 | [13.045] | 0.878 | 0.878 | 0.878 |  |
|  | L | 3.138 | [20.245] | 0.878 | 0.878 | 0.878 |  |
|  | M | 3.960 | [25.548] | 0.878 | 0.878 | 0.878 |  |
| 6252 | N | 4.774 | [30.800] | 0.878 | 0.878 | 0.878 |  |
|  | P | 7.018 | [45.277] | 0.878 | 0.878 | 0.878 |  |
|  | Q | 12.155 | [78.419] | 0.878 | 0.878 | 0.878 |  |
|  | R | 17.600 | [113.548] | 0.878 | 0.878 | 0.878 |  |

KUNKLE SAFETY AND RELIEF PRODUCTS
TECHNICAL REFERENCE

## Valve Sizing

Table B - Steam Super Heat Correction Factor, $\mathrm{K}_{\text {sh }}$

| Set Pressure psig [barg] |  | SaturatedSteamTemp. ${ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right]$ |  | Total Steam Temperature ${ }^{\circ} \mathrm{F}$ [ ${ }^{\circ} \mathrm{C}$ ] |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 280 \\ {[138]} \end{gathered}$ | $\begin{gathered} 300 \\ {[149]} \end{gathered}$ | $\begin{gathered} 320 \\ {[160]} \end{gathered}$ | $\begin{gathered} 340 \\ {[171]} \end{gathered}$ | $\begin{gathered} 360 \\ {[182]} \end{gathered}$ | $\begin{gathered} 380 \\ {[193]} \end{gathered}$ | $\begin{gathered} 400 \\ {[205]} \end{gathered}$ | $\begin{gathered} 420 \\ {[216]} \end{gathered}$ | $\begin{gathered} 440 \\ {[227]} \end{gathered}$ | $\begin{gathered} 460 \\ {[238]} \end{gathered}$ | $\begin{gathered} 480 \\ {[249]} \end{gathered}$ | $\begin{gathered} 500 \\ {[260]} \end{gathered}$ | $\begin{gathered} 520 \\ {[271]} \end{gathered}$ | $\begin{gathered} 540 \\ {[282]} \end{gathered}$ | $\begin{gathered} 560 \\ {[293]} \end{gathered}$ |
| 15 | [1.03] |  |  | 250 | [121] | 1.00 | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 98 | . 97 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 | . 90 |
| 20 | [1.38] | 259 | [126] | 1.00 | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 98 | . 97 | . 96 | . 95 | 94 | 93 | . 92 | . 91 | 90 |
| 40 | [2.76] | 287 | [142] |  | 1.00 | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 97 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 | . 90 |
| 60 | [4.14] | 308 | [153] |  |  | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 97 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 | . 90 |
| 80 | [5.52] | 324 | [162] |  |  |  | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 97 | . 96 | . 94 | . 93 | . 92 | . 91 | . 90 |
| 100 | [6.90] | 338 | [170] |  |  |  |  | 1.00 | 1.00 | . 99 | . 98 | . 97 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 |
| 120 | [8.27] | 350 | [177] |  |  |  |  | 1.00 | 1.00 | . 99 | . 98 | . 97 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 |
| 140 | [9.65] | 361 | [183] |  |  |  |  |  | 1.00 | 1.00 | . 99 | . 98 | . 96 | . 95 | . 94 | . 93 | . 92 | . 91 |
| 160 | [11.0] | 371 | [188] |  |  |  |  |  | 1.00 | 1.00 | . 99 | . 98 | . 97 | 95 | . 94 | . 93 | . 92 | 91 |
| 180 | [12.4] | 380 | [193] |  |  |  |  |  |  | 1.00 | . 99 | . 98 | . 97 | . 96 | . 95 | . 93 | . 92 | . 91 |
| 200 | [13.8] | 388 | [198] |  |  |  |  |  |  | 1.00 | . 99 | . 99 | . 97 | . 96 | . 95 | . 93 | . 92 | . 91 |
| 220 | [15.2] | 395 | [202] |  |  |  |  |  |  | 1.00 | 1.00 | 9 | . 98 | 96 | 95 | . 94 | . 93 | 92 |
| 240 | [16.6] | 403 | [206] |  |  |  |  |  |  |  | 1.00 | . 99 | . 98 | . 97 | . 95 | . 94 | . 93 | . 92 |
| 260 | [17.9] | 409 | [210] |  |  |  |  |  |  |  | 1.00 | . 99 | . 98 | . 97 | . 96 | . 94 | . 93 | . 92 |
| 280 | [19.3] | 416 | [213] |  |  |  |  |  |  |  | 1.00 | 1.00 | . 98 | . 97 | 96 | . 95 | . 93 | . 92 |
| 300 | [20.7] | 422 | [217] |  |  |  |  |  |  |  |  | 1.00 | . 99 | . 98 | . 96 | . 95 | . 93 | . 92 |
| 350 | [24.1] | 436 | [225] |  |  |  |  |  |  |  |  | 1.00 | 1.00 | . 99 | . 96 | . 96 | . 94 | . 93 |
| 400 | [27.6] | 448 | [231] |  |  |  |  |  |  |  |  |  | 1.00 | 99 | 96 | . 96 | . 95 | . 93 |
| 450 | [31.0] | 460 | [238] |  |  |  |  |  |  |  |  |  |  | 1.00 | 96 | . 96 | . 96 | . 94 |
| 500 | [34.5] | 470 | [243] |  |  |  |  |  |  |  |  |  |  | 1.00 | 96 | . 96 | . 96 | . 94 |
| 550 | [37.9] | 480 | [249] |  |  |  |  |  |  |  |  |  |  |  | 97 | . 97 | . 97 | . 95 |
| 600 | [41.4] | 489 | [254] |  |  |  |  |  |  |  |  |  |  |  | 97 | . 97 | . 97 | . 97 |
| 650 | [44.8] | 497 | [258] |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | . 99 | . 97 |
| 700 | [48.3] | 506 | [263] |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | . 99 | . 97 |
| 750 | [51.7] | 513 | [267] |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | 1.00 | . 98 |
| 800 | [55.2] | 520 | [271] |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | . 99 |
| 850 | [58.6] | 527 | [275] |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | . 99 |
| 900 | [62.1] | 533 | [278] |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 | 1.00 |
| 950 | [65.5] | 540 | [282] |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 |
| 1000 | [69.0] | 546 | [286] |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 |
| 1050 | [72.4] | 552 | [289] |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.00 |
| 1100 | [75.9] | 558 | [292] |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1150 | [79.3] | 563 | [295] |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1200 | [82.7] | 569 | [298] |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Note:

Revised capacity for "Super Heat Steam:" multiply capacity of Valve x Factor noted above.

## Valve Sizing

Table B - Steam Super Heat Correction Factor, $\mathrm{K}_{\text {sh }}$

| Set | Saturated Steam Temp. ${ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right]$ |  | Total Steam Temperature ${ }^{\circ} \mathrm{F}\left[{ }^{\circ} \mathrm{C}\right]$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pressure psig [barg] |  |  | $\begin{gathered} 580 \\ {[305]} \end{gathered}$ | $\begin{gathered} 600 \\ {[316]} \end{gathered}$ | $\begin{gathered} 620 \\ {[326]} \end{gathered}$ | $\begin{gathered} 640 \\ {[338]} \end{gathered}$ | $\begin{gathered} 660 \\ {[349]} \end{gathered}$ | $\begin{gathered} 680 \\ {[360]} \end{gathered}$ | $\begin{gathered} 700 \\ {[371]} \end{gathered}$ | $\begin{gathered} 720 \\ {[382]} \end{gathered}$ | $\begin{gathered} 740 \\ {[393]} \end{gathered}$ | $\begin{gathered} 760 \\ {[405]} \end{gathered}$ | $\begin{gathered} 780 \\ {[416]} \end{gathered}$ | $\begin{gathered} 800 \\ {[427]} \end{gathered}$ | $\begin{gathered} 900 \\ {[482]} \end{gathered}$ | $\begin{gathered} 1000 \\ {[537]} \end{gathered}$ | $\begin{gathered} 1100 \\ {[593]} \end{gathered}$ |
| 15 [1.03] | 250 | [121] | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 83 | . 82 | . 81 | . 81 | . 78 | . 75 | . 72 |
| 20 [1.38] | 259 | [126] | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 83 | . 82 | . 81 | . 81 | . 78 | . 75 | . 72 |
| 40 [2.40] | 287 | [142] | . 89 | . 88 | . 87 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 60 [4.14] | 308 | [153] | . 89 | . 88 | . 87 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 80 [5.52] | 324 | [162] | . 89 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 100 [6.90] | 338 | [170] | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 85 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 120 [8.27] | 350 | [177] | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 85 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 140 [9.65] | 361 | [183] | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 85 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 160 [11.0] | 371 | [188] | . 90 | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 180 [12.4] | 380 | [193] | . 90 | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 82 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 200 [13.8] | 388 | [198] | . 90 | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 83 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 220 [15.2] | 395 | [201] | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 8 | . 83 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 240 [16.6] | 403 | [206] | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 260 [17.9] | 409 | [209] | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 85 | . 84 | . 83 | . 82 | . 81 | . 78 | . 75 | . 72 |
| 280 [19.3] | 416 | [213] | . 91 | . 90 | . 91 | . 88 | . 87 | . 86 | . 85 | . 85 | . 84 | . 83 | . 82 | . 82 | . 78 | . 75 | . 72 |
| 300 [20.7] | 422 | [217] | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 82 | . 82 | . 78 | . 75 | . 72 |
| 350 [24.1] | 436 | [224] | . 92 | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 83 | . 83 | . 82 | . 78 | . 76 | . 72 |
| 400 [27.6] | 448 | [231] | . 92 | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 82 | . 79 | . 76 | . 72 |
| 450 [31.0] | 460 | [238] | . 93 | . 92 | . 91 | . 89 | . 88 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 82 | . 79 | . 76 | . 72 |
| 500 [34.5] | 470 | [243] | . 93 | . 92 | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 83 | . 82 | . 79 | . 76 | . 73 |
| 550 [37.9] | 480 | [249] | . 94 | . 92 | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 83 | . 82 | . 79 | . 76 | . 73 |
| 600 [41.4] | 489 | [254] | . 94 | . 93 | . 92 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 84 | . 83 | . 79 | . 76 | . 73 |
| 650 [44.8] | 497 | [258] | . 95 | . 94 | . 92 | . 91 | . 90 | . 89 | . 87 | . 86 | . 86 | . 85 | . 84 | . 83 | . 79 | . 76 | . 73 |
| 700 [48.3] | 506 | [263] | . 96 | . 94 | . 93 | . 91 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 83 | . 79 | . 76 | . 73 |
| 750 [51.7] | 513 | [267] | . 96 | . 95 | . 93 | . 92 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 83 | . 79 | . 76 | . 73 |
| 800 [55.2] | 520 | [271] | . 97 | . 95 | . 94 | . 92 | . 91 | . 90 | . 88 | . 87 | . 86 | . 85 | . 84 | . 84 | . 80 | . 76 | . 73 |
| 850 [58.6] | 527 | [275] | . 98 | . 96 | . 94 | . 93 | . 92 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 80 | . 76 | . 73 |
| 900 [62.1] | 533 | [278] | . 99 | . 97 | . 95 | . 93 | . 92 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 80 | . 77 | . 73 |
| 950 [65.5] | 540 | [282] | . 99 | . 97 | . 95 | . 94 | . 92 | . 91 | . 89 | . 88 | . 87 | . 86 | . 85 | . 84 | . 80 | . 77 | . 73 |
| 1000 [69.0] | 546 | [286] | . 99 | . 98 | . 96 | . 94 | . 93 | . 91 | . 90 | . 89 | . 87 | . 86 | . 85 | . 84 | . 80 | . 77 | . 73 |
| 1050 [72.4] | 552 | [289] | 1.00 | . 99 | . 97 | . 95 | . 93 | . 92 | . 90 | . 89 | . 88 | . 87 | . 86 | . 85 | . 80 | . 77 | . 73 |
| 1100 [75.9] | 558 | [292] | 1.00 | . 99 | . 98 | . 95 | . 94 | . 92 | . 91 | . 89 | . 88 | . 87 | . 86 | . 85 | . 81 | . 77 | . 73 |
| 1150 [79.3] | 563 | [295] | 1.00 | . 99 | . 98 | . 96 | . 94 | . 92 | . 91 | . 90 | . 88 | . 87 | . 86 | . 85 | . 81 | . 77 | . 73 |
| 1200 [82.7] | 569 | [298] | 1.00 | . 99 | . 98 | . 97 | . 95 | . 93 | . 91 | . 90 | . 89 | . 87 | . 86 | . 85 | . 81 | . 77 | . 73 |

## Note:

Revised capacity for "Super Heat Steam:" multiply capacity of Valve $\times$ Factor noted above.

KUNKLE SAFETY AND RELIEF PRODUCTS
TECHNICAL REFERENCE

## Valve Sizing

Table C - Air and Gas Temperature Correction Factors

| Temperature ${ }^{\circ} \mathrm{F}$ | Tc | Temperature ${ }^{\circ} \mathrm{F}$ | Tc | Temperature ${ }^{\circ} \mathrm{F}$ | Tc | Temperature ${ }^{\circ} \mathrm{F}$ | Tc |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.062 | 90 | 0.972 | 260 | 0.849 | 440 | 0.760 |
| 10 | 1.051 | 100 | 0.964 | 280 | 0.838 | 460 | 0.752 |
| 20 | 1.041 | 120 | 0.947 | 300 | 0.828 | 480 | 0.744 |
| 30 | 1.030 | 140 | 0.931 | 320 | 0.817 | 500 | 0.737 |
| 40 | 1.020 | 160 | 0.916 | 340 | 0.806 | 550 | 0.718 |
| 50 | 1.009 | 180 | 0.902 | 360 | 0.796 | 600 | 0.701 |
| 60 | 1.000 | 200 | 0.888 | 380 | 0.787 | 650 | 0.685 |
| 70 | 0.991 | 220 | 0.874 | 400 | 0.778 | 700 | 0.669 |
| 80 | 0.981 | 240 | 0.862 | 420 | 0.769 | 750 | 0.656 |

For temperatures other than $60^{\circ} \mathrm{F}$ at valve inlet, multiply standard SCFM by Tc.

Table D - Gas and Liquid Relative Density Correction Factors

| Specific Gravity | Dc | Specific Gravity | Dc | Specific Gravity | Dc | Specific Gravity | Dc |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.07 | 3.770 | 0.60 | 1.290 | 1.05 | 0.975 | 1.70 | 0.768 |
| 0.08 | 3.530 | 0.65 | 1.240 | 1.10 | 0.955 | 1.80 | 0.745 |
| 0.09 | 3.333 | 0.70 | 1.195 | 1.15 | 0.933 | 1.90 | 0.725 |
| 0.10 | 3.160 | 0.75 | 1.155 | 1.20 | 0.913 | 2.00 | 0.707 |
| 0.20 | 2.240 | 0.80 | 1.117 | 1.25 | 0.895 | 2.50 | 0.633 |
| 0.30 | 1.825 | 0.85 | 1.085 | 1.30 | 0.877 | 3.00 | 0.577 |
| 0.40 | 1.580 | 0.90 | 1.055 | 1.40 | 0.845 | 3.50 | 0.535 |
| 0.50 | 1.414 | 0.95 | 1.025 | 1.50 | 0.817 | 4.00 | 0.500 |
| 0.55 | 1.350 | 1.00 | 1.000 | 1.60 | 0.791 | 4.50 | 0.471 |

For a specific gravity other than air or water (=1.0), multiply CFM or GPM by Dc.

## Valve Sizing

| Physical Properties |  |  |
| :--- | :---: | :---: |
| Gas or Vapor | M <br> Molecular <br> Weight | kpecific <br> Heat Ratio |
| Gas Constant |  |  |

KUNKLE SAFETY AND RELIEF PRODUCTS
TECHNICAL REFERENCE

## Valve Sizing

## Physical Properties

| Gas or Vapor | M <br> Molecular Weight | k Specific Heat Ratio | $\stackrel{\text { C }}{\text { Gas Constant }}$ |
| :---: | :---: | :---: | :---: |
| Hexane | 86.18 | 1.06 | 322 |
| Hydrogen | 2.02 | 1.41 | 357 |
| Hydrogen Chloride, Anhydrous | 36.46 | 1.41 | 357 |
| Hydrogen Sulfide | 34.08 | 1.32 | 349 |
| Isobutane (2-Methylpropane) | 58.12 | 1.10 | 327 |
| Isoprene (2-Methyl-1, 3 Butadiene) | 68.12 | 1.09 | 326 |
| Isopropyl Alcohol (Isopropanol) | 60.10 | 1.09 | 326 |
| Krypton | 83.80 | 1.71 | 380 |
| Methane | 16.04 | 1.31 | 348 |
| Methyl Alcohol (Methanol) | 32.04 | 1.20 | 337 |
| Methylamines, Anhydrous |  |  |  |
| Monomethylamine (Methylamine) | 31.06 | 1.02 | 317 |
| Dimethylamine | 45.08 | 1.15 | 332 |
| Trimethylamine | 59.11 | 1.18 | 335 |
| Methyl Mercapton (Methanethiol) | 48.11 | 1.20 | 337 |
| Naphthalene (Napthaline) | 128.17 | 1.07 | 323 |
| Natural Gas (specific gravity $=0.60$ ) | 17.40 | 1.27 | 344 |
| Neon | 20.18 | 1.64 | 375 |
| Nitrogen | 28.01 | 1.40 | 356 |
| Nitrous Oxide | 44.01 | 1.30 | 347 |
| Octane | 114.23 | 1.05 | 321 |
| Oxygen | 32.00 | 1.40 | 356 |
| Pentane | 72.15 | 1.07 | 323 |
| Propadiene (Allene) | 40.07 | 1.69 | 379 |
| Propane | 44.10 | 1.13 | 330 |
| Propylene (Propene) | 42.08 | 1.15 | 332 |
| Propylene Oxide | 58.08 | 1.13 | 330 |
| Styrene | 104.15 | 1.07 | 323 |
| Sulfur Dioxide | 64.06 | 1.28 | 345 |
| Sulfur Hexafluoride | 146.05 | 1.09 | 326 |
| Steam | 18.02 | 1.31 | 348 |
| Toluene (Toluol or Methylbenzene) | 92.14 | 1.09 | 326 |
| Triethylene Glycol (TEG) | 150.18 | 1.04 | 320 |
| Vinyl Chloride Monomer (VCM) | 62.50 | 1.19 | 336 |
| Xenon | 131.30 | 1.65 | 376 |
| Xylene (p-Xylene) | 106.17 | 1.07 | 323 |

KUNKLE SAFETY AND RELIEF PRODUCTS
TECHNICAL REFERENCE

## Valve Sizing

## Physical Properties

| Liquid | G Specific Gravity Water = 1 | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: |
| Acetaldehyde | 0.779 | 68 | 20 |
| Acetic Acid | 1.051 | 68 | 20 |
| Acetone | 0.792 | 68 | 20 |
| Ammonia, Anhydrous | 0.666 | 68 | 20 |
| Automotive Crankcase and Gear Oils: |  |  |  |
| SAE-5W Through SAE 150 | 0.88-0.94 | 60 | 15.6 |
| Beer | 1.01 | 60 | 15.6 |
| Benzene (Benzol) | 0.880 | 68 | 20 |
| Boron Trifluoride | 1.57 | -148 | -100 |
| Butadiene - 1, 3 | 0.622 | 68 | 20 |
| Butane-n (Normal Butane) | 0.579 | 68 | 20 |
| Butylene (1-Butene) | 0.600 | 68 | 20 |
| Carbon Dioxide | 1.03 | -4 | -20 |
| Carbon Disulfide (C. Bisulfide) | 1.27 | 68 | 20 |
| Carbon Tetrachloride | 1.60 | 68 | 20 |
| Chlorine | 1.42 | 68 | 20 |
| Chloromethane (Methyl Chloride) | 0.921 | 68 | 20 |
| Crude Oils: |  |  |  |
| 32.6 Deg API | 0.862 | 60 | 15.6 |
| 35.6 Deg API | 0.847 | 60 | 15.6 |
| 40 Deg API | 0.825 | 60 | 15.6 |
| 48 Deg API | 0.79 | 60 | 15.6 |
| Cyclohexane | 0.780 | 68 | 20 |
| Cyclopropane (Trimethylene) | 0.621 | 68 | 20 |
| Decane-n | 0.731 | 68 | 20 |
| Diesel Fuel Oils | 0.82-0.95 | 60 | 15.6 |
| Diethylene Glycol (DEG) | 1.12 | 68 | 20 |
| Dimethyl Ether (Methyl Ether) | 0.663 | 68 | 20 |
| Dowtherm A | 0.998 | 68 | 20 |
| Dowtherm E | 1.087 | 68 | 20 |
| Ethane | 0.336 | 68 | 20 |
| Ethyl Alcohol (Ethanol) | 0.79 | 68 | 20 |
| Ethylene (Ethene) | 0.569 | -155 | -104 |
| Ethylene Glycol | 1.115 | 68 | 20 |
| Ethylene Oxide | 0.901 | 68 | 20 |

KUNKLE SAFETY AND RELIEF PRODUCTS
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## Valve Sizing

| Physical Properties |  |  |  |
| :--- | :--- | :--- | :--- |
| Liquid | G <br> Specific Gravity <br> Water = 1 | ${ }^{\circ}$ F | o |
|  |  |  |  |
| Fluorocarbons: | 68 | 20 |  |
| R12, Dichlorodifluoromethane | 1.34 | 20 |  |
| R13, Chlorotrifluoromethane | 0.916 | 68 | 20 |
| R13B1, Bromotrifluoromethane | 1.58 | 68 | 20 |
| R22, Chlorodifluoromethane | 1.21 | 68 | 20 |
| R115, Chloropentafluoromethane | 1.31 | 68 | 15.6 |
| Fuel Oils, Nos. 1, 2, 3, 5 and 6 | $0.82-0.95$ | 60 | 15.6 |
| Gasolines | $0.68-0.74$ | 60 | 20 |
| Glycerine (Glycerin or Glycerol) | 1.26 | 68 | 20 |
| Heptane | 0.685 | 68 | 20 |
| Hexane | 0.660 | 68 | 15.6 |
| Hydrochloric Acid | 1.64 | 60 | 20 |
| Hydrogen Sulfide | 0.78 | 68 | 20 |
| Isobutane (2-Methylpropane) | 0.558 | 68 | 20 |
| Isoprene (2-Methyl - 1, 3-Butadiene) | 0.682 | 68 | 20 |
| Isopropyl Alcohol (Isopropanol) | 0.786 | 68 | 15.6 |
| Jet Fuel (average) | 0.82 | 60 | 15.6 |
| Kerosene | $0.78-0.82$ | 60 | 20 |
| Methyl Alcohol (Methanol) | 0.792 | 68 |  |
| Methylamines, Anhydrous: |  | 68 | 20 |
| Monomethylamine (Methylamine) | 0.663 | 68 | 20 |
| Dimethylamine | 0.656 | 68 | 20 |
| Trimethylamine | 0.634 | 68 | 20 |
| Methyl Mercapton (Methanethiol) | 0.870 | 68 | 20 |
| Nitric Acid | 1.50 | 60 | 15.6 |
| Nitrous Oxide | 1.23 | -127 | -88.5 |
| Octane | 0.703 | 68 | 20 |
| Pentane | 0.627 | 68 | 20 |
| Propadiene (Allene) | 0.659 | -30 | -34.4 |
| Propane | 0.501 | 68 | 20 |
| Propylene (Propene) | 0.514 | 68 | 20 |
| Propylene Oxide | 0.830 | 68 | 20 |
| Styrene | 0.908 | 68 | 20 |
| Sulfur Dioxide | 1.43 | 68 | 20 |
|  |  |  |  |

## Valve Sizing

Physical Properties
G

| Liquid | Specific Gravity <br> Water = | ${ }^{\circ} \mathbf{F}$ | ${ }^{\circ} \mathbf{C}$ |
| :--- | :---: | :---: | :---: |
| Sulfur Hexafluoride | 1.37 | 68 | 20 |
| Sulfuric Acid: | 1.839 | 68 | 20 |
| 95-100\% | 1.50 | 68 | 20 |
| 60\% | 1.14 | 68 | 20 |
| 20\% | 0.868 | 68 | 20 |
| Toluene (Toluol or Methylbenzene) | 1.126 | 68 | 20 |
| Triethylene Glycol (TEG) | 0.985 | -4 | -20 |
| Vinyl Chloride Monomer (VCM) | 1.00 | 68 | 20 |
| Water, fresh | 1.03 | 68 | 20 |
| Water, sea | 0.862 | 68 | 20 |
| Xylene (p-Xylene) |  |  |  |

## Sizing - Determining $\mathrm{K}_{\mathrm{v}}$ and $\mathrm{K}_{\mathrm{w}}$

## U.S. Units

$$
\begin{aligned}
& \mathrm{R}=\frac{\mathrm{V}_{\mathrm{L}}(2,800 \mathrm{G})}{\mu \sqrt{\mathrm{A}}} \\
& \text { or } \\
& \mathrm{R}=\frac{12,700 \mathrm{~V}_{\mathrm{L}}}{\mathrm{U} \sqrt{\mathrm{~A}}}
\end{aligned}
$$

## Metric Units

$$
R=\frac{31,313 V_{L} G}{\mu \sqrt{A}}
$$

## Determining $\mathrm{K}_{\mathrm{v}}$

$V_{L}=$ Flow rate at the flowing temperature, in U.S. gpm [m $3 / \mathrm{hr}$ ]
$V_{L}=$ Flow rate at the flowing temperature, in U.S. gpm [m $3 / \mathrm{hr}$ ]

G = Specific gravity of liquid at flowing temperature referred to water $=1.00$ at $70^{\circ} \mathrm{F}\left[21^{\circ} \mathrm{C}\right]$
$\mu=$ Absolute viscosity at the flowing temperature, in centipoises

A = Effective discharge area, in square inches [cm²] (from manufacturer's standard orifice areas)
$U=$ Viscosity at the flowing temperature, in Saybolt Universal seconds

After the value of $R$ is determined, the factor $K_{v}$ is obtained from the graph. Factor $K_{v}$ is applied to correct the "preliminary required discharge area." If the corrected area exceeds the "chosen standard orifice area," the calculations should be repeated using the next larger standard orifice size.


R = Reynolds Number

KUNKLE SAFETY AND RELIEF PRODUCTS
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## Conversion Factors

| Absolute Viscosity |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Given | To find desired value, multiply "Given" value by factor below |  |  |  |
|  | poise | Centipoise | $\frac{\mathrm{gm}}{\mathrm{~cm}-\mathrm{sec}}$ | $\frac{\mathrm{lb}}{\mathrm{ft}-\mathrm{sec}}$ |
| poise | - | 100 | 1 | 0.0672 |
| centipoise | 0.01 | - | 0.01 | 0.000672 |
| $\frac{\mathrm{gm}}{\mathrm{~cm}-\mathrm{sec}}$ | 1 | 100 | - | 0.0672 |
| $\frac{\mathrm{lb}}{\mathrm{ft}-\mathrm{sec}}$ | 14.88 | 1488 | 14.88 | - |

Kinematic Viscosity
Given

|  | stoke | Centistoke | $\frac{\mathbf{c m}^{2}}{\mathbf{s e c}}$ | $\frac{\mathbf{s t 2}}{\mathbf{s e c}}$ |
| :---: | :---: | :---: | :---: | :---: |
| stoke | - | 100 | 1 | 0.001076 |
| centistoke | 0.01 | - | 0.01 | $1.076 \times 10-5$ |
| $\frac{\mathrm{~cm}^{2}}{\mathrm{sec}}$ | 1 | 100 | - | 0.001076 |
| $\frac{\mathrm{ft}^{2}}{\mathrm{sec}}$ | 929.0 | 92900 | 929.0 | - |

## Liquid Flow Conversions

| Given | To find desired value, multiply "Given" value by factor below |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | l/hr | gpm - US | gpm - Imp | barrels/day | $\mathrm{m}^{3} / \mathrm{hr}$ |
| l/hr (litres/hour) | - | 0.00440 | 0.003666 | 0.1510 | 0.0010 |
| gpm (US gallons per minute) | 227.1 | - | 0.8327 | 34.29 | 0.2271 |
| $\begin{gathered} \text { gpm } \\ \text { (Imperial gallons per minute) } \end{gathered}$ | 272.8 | 1.201 | - | 41.18 | 0.2728 |
| barrels/day (petroleum - 42 US gallons) | 6.624 | 0.02917 | 0.02429 | - | 0.006624 |
| $\mathrm{m}^{33} / \mathrm{hr}$ (cubic meters per hour) | 1000 | 4.403 | 3.666 | 151.0 | - |
| $\mathrm{m}^{3} / \mathrm{s}$ <br> (cubic meters per second) | $3.6 \times 10^{6}$ | 0.02917 | 0.02429 | - | 0.006624 |
| kg/hr (kilograms per hour) | $\frac{1}{G}$ | $\frac{1}{227.1 G}$ | $\frac{1}{272.8 G}$ | $\frac{0.151}{G}$ | $\frac{1}{1000 G}$ |
| lb/hr (pounds per hour) | $\frac{1}{2.205 G}$ | $\frac{1}{500.8 \mathrm{G}}$ | $\frac{1}{601.5 G}$ | $\frac{1}{14.61 G}$ | $\frac{1}{2205 G}$ |

## Notes:

1. Kinematic viscosity $\times$ specific gravity $=$ absolute viscosity
2. Centistokes $x$ specific gravity $=$ centipoise .
3. Saybolt Second Universal (SSU) $\times 0.216 \times$ specific gravity = centipoise.

## Note:

1. $G=$ Specific gravity of liquid at its relieving temperature compared to that of water at $68^{\circ} \mathrm{F}\left[20^{\circ} \mathrm{C}\right]$, where Gwater $=1.00$.

## Conversion Factors

## Gas Flow Conversions

| Given | To find desired value, multiply "Given" value by factor below |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SCFM | SCFH | lb/hr | [kg/hr] | [ $\mathrm{Nm}^{3} / \mathrm{hr}$ ] | [ $\mathrm{Nm}^{3} / \mathrm{min}$ ] |
| scfm2 | - | 60 | $\frac{M}{6.32}$ | $\frac{M}{13.93}$ | 1.608 | 0.0268 |
| scfh2 | 0.01677 | - | $\frac{\mathrm{M}}{379.2}$ | $\frac{\mathrm{M}}{836.1}$ | 0.0268 | 0.000447 |
| lb/hr3 or \#/hr3 | $\frac{6.32}{M}$ | $\frac{379.2}{M}$ | - | 0.4536 | $\frac{10.17}{M}$ | $\frac{0.1695}{M}$ |
| kg/hr4 | $\frac{13.93}{M}$ | $\frac{836.1}{M}$ | 2.205 | - | $\frac{22.40}{M}$ | $\frac{0.3733}{M}$ |
| Nm3/hr 5 | 0.6216 | 37.30 | $\frac{\mathrm{M}}{10.17}$ | $\frac{M}{22.40}$ | - | 0.01667 |
| $\mathrm{Nm} 3 / \mathrm{min} 5$ | 37.30 | 2238 | 5.901 M | 2.676 M | 60 | - |

If flow is expressed in actual volume, such as cfm (cubic feet per minute) or acfm (actual cfm) as is often done for compressors, where the flow is described as

## Inch-Pound Units

SCFM $=\left(\begin{array}{c}\operatorname{cfm} \\ \mathrm{Or} \\ \mathrm{acfm}\end{array}\right) \times \frac{14.7+\mathrm{p}}{14.7} \times \frac{520}{460+\mathrm{t}}$
Where:
$p=$ gauge pressure of gas or vapor in psig
$t=$ temperature of gas or vapor in ${ }^{\circ} \mathrm{F}$
displacement or swept volume, the flow
may be converted to scfm as follows (or from flow expressed in $\mathrm{m}^{3} / \mathrm{hr}$ to $\mathrm{Nm}^{3} / \mathrm{hr}$ ).

## Metric Units

$\mathrm{Nm}^{3} / \mathrm{hr}=\mathrm{m}^{3} \mathrm{hr}=x \frac{1.013+\mathrm{p}}{1.013} \times \frac{273}{273+\mathrm{t}}$
Where:
$p=$ gauge pressure of gas or vapor in barg $t=$ temperature of gas or vapor in ${ }^{\circ} \mathrm{C}$

## Pressure Conversion

| Given | To find desired value, multiply "Given" value by factor below |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| kPa (kilopascal) | - | 0.1450 | 0.0102 | 0.0100 |
| psig (pounds/in2)3 | 6.895 | - | 0.0703 | 0.06895 |
| kg/cm2 ${ }^{(1)}$ (kilograms/cm²) | 98.07 | 14.22 | - | 0.9807 |
| barg | 100.00 | 14.50 | 1.020 | - |

## Area Conversion

| Given | To find desired value, multiply "Given" value by factor below |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| in2 | - | 0.006944 | 645.16 | 6.4516 |
| cm ${ }^{2}$ | 0.155 | $1.076 \times 10^{-3}$ | 100 | - |
| $\mathrm{ft}^{2}$ | 144 | - | 92900 | 929 |
| mm² | 0.00155 | $1.076 \times 10^{-5}$ | - | 0.01 |

## Temperature Conversion

| Degrees Celsius ( ${ }^{\circ} \mathrm{C}$ ) | Degrees Fahrenheit ( ${ }^{\circ} \mathrm{F}$ ) |
| :---: | :---: |
| $\mathrm{C}+273.15=\mathrm{K}$ (Kelvin) | $\mathrm{F}+459.67=\mathrm{R}$ (Rankine) |
| $(\mathrm{C} \times 1.8)+32=\mathrm{F}$ (Fahrenheit) | $(\mathrm{F}-32) \times 0.556=\mathrm{C}$ (Celsius) |

## Notes:

1. $M=$ Molecular weight of vapor or gas.
2. Volumetric flow (per time unit of hour or minute as shown) in standard cubic feet per minute at 14.7 psia [ 1.013 bara], $60^{\circ} \mathrm{F}$ [16 ${ }^{\circ} \mathrm{C}$ ].
3. Weight flow in pounds per hour.
4. Weight flow in kilograms per hour.
5. Volumetric flow (per time unit of hour or minute as shown) at 1.013 bara $32^{\circ} \mathrm{F}\left[0^{\circ} \mathrm{C}\right]$. This represents the commercial standard, known as the Normal Temperature and Pressure (NTP).

Conversions from one volumetric flow rate to another or to weight flow (and vice versa) may only be done when the volumetric flow is expressed in the standard conditions shown above. If flows are expressed at temperature or pressure bases that differ from those listed above, they must first be converted to the standard base.

## Notes:

1. Also expressed as $\mathrm{kp} / \mathrm{cm}^{2}$ and $\mathrm{kgf} / \mathrm{cm}^{2}$.
2. Normal Temperature and Pressure (NTP) Conditions are, at sea level, equal to 1.013 bara or $1.033 \mathrm{~kg} / \mathrm{cm}^{2}$ (kilograms force per square centimeter absolute) at a base temperature of $32^{\circ} \mathrm{F}\left[0^{\circ} \mathrm{C}\right]$. This differs slightly from Metric Standard Conditions (MSC), which uses 1.013 bara $60^{\circ} \mathrm{F}\left[15^{\circ} \mathrm{C}\right]$ for the base temperature.
3. Inch-Pound Standard Conditions are, at sea level, equal to 14.7 psia (pounds force per square inch absolute), rounded up from 14.696 psia, and at a base temperature of $60^{\circ} \mathrm{F}$ $\left[16^{\circ} \mathrm{C}\right]$.

## Installation

1. Before installing a new safety/relief valve, we recommend that a pipe tap be used to assure clean-cut and uniform threads in the vessel opening and to allow for normal hand engagement followed by a half to one turn by wrench.
2. Install the valve in a vertical position so that discharge piping and code required drains can be properly piped to prevent build-up of back pressure and accumulation of foreign material around the valve seat area.
3. Avoid over-tightening as this can distort safety/relief valve seats. One need only remember that as the vessel and valve are heated, the expansion involved will grasp the valve more firmly.
4. When installing flange connected valves, use new gaskets and draw the mounting bolts down evenly.
5. Do not use the valve outlet or cap as a lever for installation. Use only flat jawed wrenches on the flats provided.
6. Avoid excessive "popping" of the safety/relief valve as even one opening can provide a means for leakage. Safety/relief valves should be operated only often enough to assure that they are in good working order.
7. Avoid wire, cable, or chain pulls for attachment to levers that do not allow a vertical pull. The weight of these devices should not be directed to the safety/relief valve.
8. Avoid having the operating pressure too near the safety/relief valve set pressure. A very minimum differential of 5 psig or 10 percent (whichever is greater) is recommended. An even greater differential is desirable, when possible, to assure better seat tightness and valve longevity. Safety/relief valves in high-temperature hot water and organic fluid service are more susceptible to damage and leakage than safety valves for steam. It is recommended that the maximum allowable working pressure of the boiler and the safety/relief valve setting be selected substantially higher than the operating pressure. A differential of $30-40$ percent is recommended.
9. Avoid discharge piping where its weight is carried by the safety/relief valve. Even though supported separately, changes in temperature alone can cause piping strain. We recommend that drip pan elbows or flexible connections be used wherever possible Isee Type A, B, C Installation, page 29).
10. Apply a moderate amount of pipe compound to male threads only, leaving the first thread clean. Compound applied to female threads or used to excess can find its way into the valve, causing leakage.

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Installation

Recommended Discharge Installation

Type " A " Installation


## Installation

## Recommended Discharge Installation

## Type "B" Installation



## Installation

## Recommended Discharge Installation

## Type "C" Installation



Pipe to Discharge $ـ$

## Maintenance

1. Develop a regular program of visual inspection, looking for clogged drains and discharge pipe, dirt build-up in and around the valve seat and broken or missing parts.
2. Test the valve every two to six months (depending on valves' age and condition) preferably by raising the system pressure to the valves set pressure or operating the hand lever (see \#3 in Operation).
3. Do not paint, oil, or otherwise cover any interior or working parts of any safety valve. They do not require any lubrication or protective coating to work properly.
When safety/relief valves require repair, service adjustments, or set pressure changes, work shall be accomplished by the manufacturer, or holders of " $V$," "UV," and/or "VR" stamps.
[^1]
[^0]:    1. Set pressures less than 15 psig [1.0 barg] are non-code only.
    2. See also ASME Section VIII steam valves for non-code steam applications.
[^1]:    5500 WAYZATA BLVD \# 800, MINNEAPOLIS, MN 55416 WWW.PENTAIR.COM/VALVES
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